



Mini-Coil Design

Michael von Ortenberg

**Fukui University, Okayama University,
Humboldt University at Berlin**

presented at

Mini Coil Workshop

IMR, Tohoku University, November 24,2006

PARAMETERS of the Mini-Coils constructed:



Coil	A	B	C	D	E
Bore (mm)	3/2.6	3/2.6	3/2.6	3/2.6	3/2.6
Wire (mm)	0.5 Cu/Ag	0.5 Cu/Ag	0.5 Cu/Ag	0.5 Cu/Ag	2x0.5 Cu/Ag
Number of layers	12	16	14	12	12
Total height (mm)	20	20	20	15	20
R ₃₀₀ (Ohm) With steel flanges	1.017	1.76	1.304	0.747	0.285
R ₃₀₀ (Ohm) Without steel flanges	-	-	-	0.728	0.285
R ₇₇ (Ohm) with steel flanges	0.257	0.371	-	-	-
L ₃₀₀ (μH) without steel flanges	-	-	-	138,7	-
L ₃₀₀ (μH) with steel flanges	292	758	549.7	182.45	86
B/U _{coil} (T/V)	2.98/100	1.30/102	2.82/101	3.64/101	3.20/103
B _{max} (T)/U _{coil}	47.78/1997	41.06/1997	46.29/1997	51.85/1806	51.72/1805
τ/2 = (t _{Bmax} - t _{B0}) (msec) at 77 K	0.74	1.03	0.886	0.564	0.414
Operation	crowbar	crowbar	crowbar	crowbar	crowbar

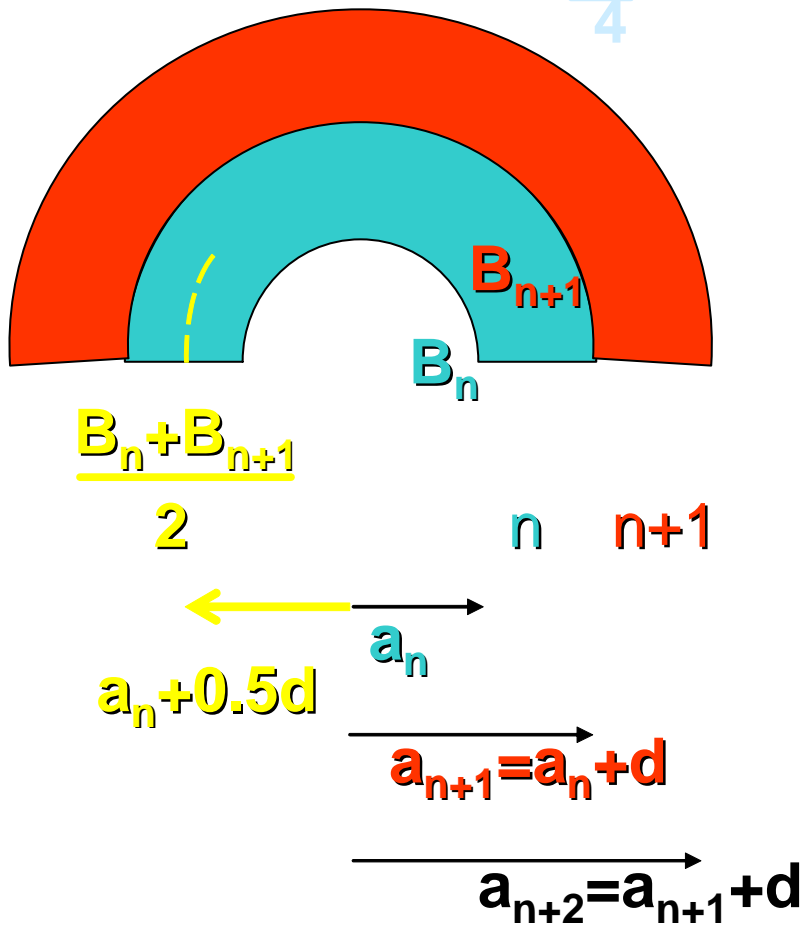
Schematic of Construction:



Schematic of Calculation:

$$B_{n+1} = B_n - \Delta B_n(a_n)$$

$$\sigma_n = \frac{(B_n + B_{n+1})}{2} * I * \frac{(a_n + 0.5d)}{\frac{\pi d^2}{4}}$$



Math-CAD Program:

*Program SpulOkayama-Sendai.mcd for the computation of MINI COILS in OKAYAMA for Cu/Ag-wire with breaking tension 0.78 G-Pa
Version 26.10.06 based on SpulNeu.mcd of 7.11.02*

$$i := \sqrt{-1}$$

Parameters:

a1 := 1.5 **[mm] inner radius of the coil**

la := 20 **[mm] total height of coil**

I0 := 1.78 **[kA] current in the wire**

Bm := 48 **[T] maximum field of coil**

d := 0.5 **[mm] diameter of wire**

pd := 9.96 **[gr/cm-3] density Cu**

NL := 12 **: number of windings**

Capacitor banks #1 and #2:

C1 := $7.2 \cdot 10^{-3}$ **Farad**

U1 := 5000 **Volt 90 kJ**

C2 := $0.96 \cdot 10^{-3}$ **Farad**

U2 := 2000 **Volt 4 kJ**

Current density in wire at maximum current:

$$j := \frac{I_0}{0.25 \cdot \pi \cdot d^2} \quad j = 9.065 \quad \text{[kA/mm}^2\text{] in wire}$$

$$j_e := \frac{I_0}{d^2} \quad j_e = 7.12 \quad \text{:[kA/mm}^2\text{] effective homogeneous current density}$$

Fieldfunctions in the homogeneous coil:

Field [T] in the coil axis at height z [mm] above the center:

a [mm] inner radius of the one-layer coil, la [mm] total height of the coil, I current in kA

$$B(z, a, la, I) := \frac{1.26 \cdot I}{2 \cdot d} \cdot \left[\frac{0.5 - \frac{z}{la}}{\sqrt{\left(0.5 - \frac{z}{la}\right)^2 + \left(\frac{a}{la}\right)^2}} + \frac{0.5 + \frac{z}{la}}{\sqrt{\left(0.5 + \frac{z}{la}\right)^2 + \left(\frac{a}{la}\right)^2}} \right] \quad \text{: for effective homogeneous current density } I_0/(d^2)$$

Field [T] at position y [mm] for z=0 inside or outside of the coil:

$$BE(y, a, la, l) := \frac{1.26 \cdot l}{2 \cdot \pi \cdot d} \int_0^\pi \frac{1 - \left(\frac{y}{a}\right) \cdot \cos(\phi)}{\left[1 + \left(\frac{y}{a}\right)^2 - 2 \cdot \left(\frac{y}{a}\right) \cdot \cos(\phi)\right] \cdot \sqrt{0.25 + \left(\frac{y}{la}\right)^2 - 1 \cdot \left(\frac{y}{la}\right) \cdot \cos(\phi) + \left(\frac{a}{la}\right)^2}} d\phi$$

Remark: $BE(y)$ has a pronounced step at the position $y=a$ and reduces to 0 for larger y .

**Fieldstrength $BF(0,y,z)$ inside and outside the coil:
y-component:**

$$BF_y(y, z, a, la, l) := \frac{-1.26 \cdot l}{2 \cdot \pi \cdot d} \int_0^\pi \frac{\cos(\phi)}{\left[\left(\frac{la}{2 \cdot a} + \frac{z}{a}\right)^2 + 1 - 2 \cdot \frac{y}{a} \cdot \cos(\phi) + \left(\frac{y}{a}\right)^2\right]^{0.5}} \dots d\phi$$

z-component:

$$+ \frac{-\cos(\phi)}{\left[\left(\frac{la}{2 \cdot a} - \frac{z}{a}\right)^2 + 1 - 2 \cdot \frac{y}{a} \cdot \cos(\phi) + \left(\frac{y}{a}\right)^2\right]^{0.5}}$$

$$BF_z(y, z, a, la, l) := \frac{-1.26 \cdot l}{2 \cdot \pi \cdot d} \int_0^\pi \frac{\left(\frac{y}{a} \cdot \cos(\phi) - 1\right) \cdot \left(\frac{la}{2 \cdot a} - \frac{z}{a}\right)}{\left[1 - 2 \cdot \frac{y}{a} \cdot \cos(\phi) + \left(\frac{y}{a}\right)^2\right] \cdot \left[\left(\frac{la}{2 \cdot a} - \frac{z}{a}\right)^2 + 1 - 2 \cdot \frac{y}{a} \cdot \cos(\phi) + \left(\frac{y}{a}\right)^2\right]^{0.5}} \dots d\phi$$

$$+ \frac{\left(\frac{y}{a} \cdot \cos(\phi) - 1\right) \cdot \left(\frac{la}{2 \cdot a} + \frac{z}{a}\right)}{\left[1 - 2 \cdot \frac{y}{a} \cdot \cos(\phi) + \left(\frac{y}{a}\right)^2\right] \cdot \left[\left(\frac{la}{2 \cdot a} + \frac{z}{a}\right)^2 + 1 - 2 \cdot \frac{y}{a} \cdot \cos(\phi) + \left(\frac{y}{a}\right)^2\right]^{0.5}}$$

Computation of the tension in element ($d \times d$) in homogeneous coil enclosing wire of diameter d :

a : inner radius of the winding considered in [mm]

d : wire diameter in [mm]

B : Magnetfield produced by the winding above the considered winding in [T],

j : Current density within the considered winding in [kA/mm²]

$$Bb_1 := Bm \quad a_1 := 1.5$$

$$n := 2 \dots NL + 1$$

$$a_n := a_{n-1} + d$$

$$Bb_n := Bb_{n-1} - B(0, a_{n-1}, la, l_0)$$

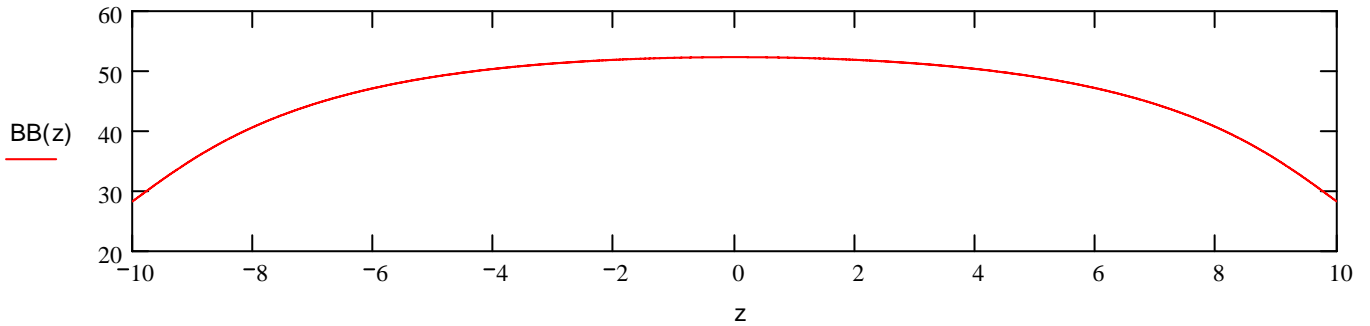
$$\sigma_{n-1} := \frac{(Bb_{n-1} + Bb_n)}{2} \cdot 10 \cdot \frac{\left(a_{n-1} + \frac{d}{2}\right)}{(d^2)} \cdot 10^{-3} \text{ : G-Pa in square element } (d \times d) \text{ in contrast to wire cross section } \pi d^2/4$$

$$\sigma_{NL+1} := \frac{Bb_{NL+1}}{2} \cdot 10 \cdot \frac{\left(a_{NL+1} + \frac{d}{2}\right)}{(d^2)} \cdot 10^{-3} \quad \sigma_{NL} = 0.033$$

Total diameter of coil: $D_{total} := 2 \cdot (a_{NL} + d)$ $D_{total} = 15$: [mm]

Calculation of the z-dependence of the field in the center axis:

$$BB(z) := \sum_{n=1}^{NL+1} B(z, a_n + 0.5 \cdot d, I_a, I_0)$$



$$\frac{BB(2)}{BB(0)} = 0.991$$

Hence within +/- 2 mm around center field inhomogeneity very small!

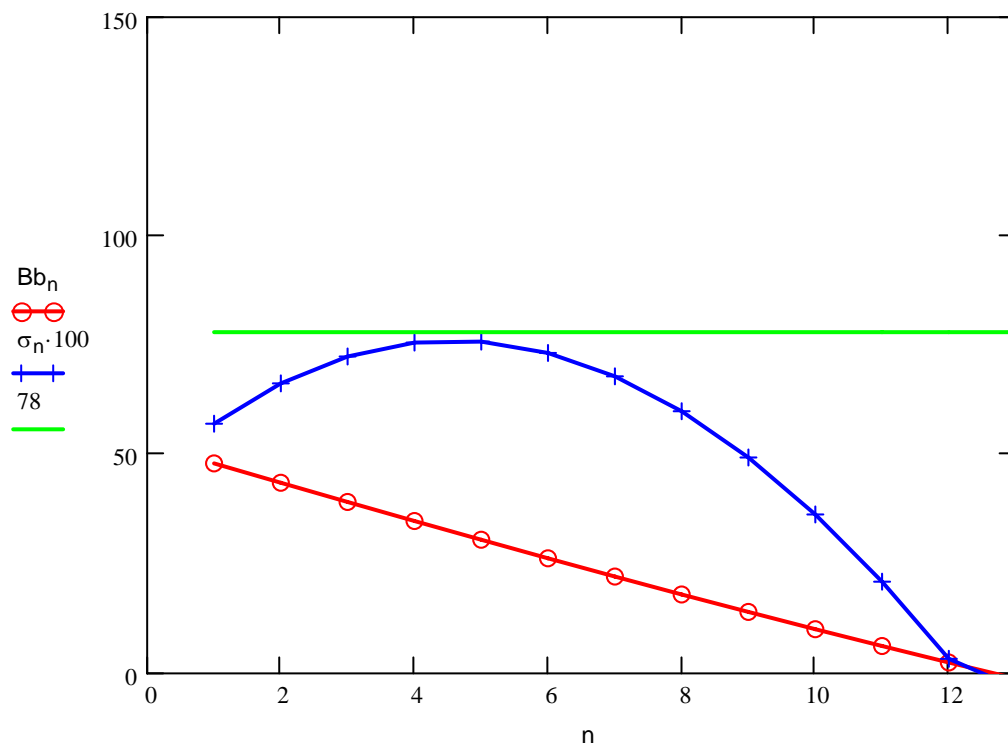
<p>Total number of windings: $NL = 12$</p>	<p>a: inner winding radius in mm</p>	<p>Bb: magnetic field inside winding in T</p>	<p>σ; strain in wire of winding in G-Pa</p>
$\begin{pmatrix} 0 \\ 1.5 \\ 2 \\ 3 \\ 3.5 \\ 4 \\ 4.5 \\ 5 \\ 5.5 \\ 6 \\ 6.5 \\ 7 \\ 7.5 \end{pmatrix}$	$\begin{pmatrix} 0 \\ 48 \\ 43.564 \\ 34.814 \\ 30.517 \\ 26.284 \\ 22.119 \\ 18.028 \\ 14.016 \\ 10.086 \\ 6.24 \\ 2.479 \\ -1.196 \end{pmatrix}$	$\begin{pmatrix} 0 \\ 0.57 \\ 0.663 \\ 0.756 \\ 0.758 \\ 0.732 \\ 0.679 \\ 0.599 \\ 0.493 \\ 0.363 \\ 0.21 \\ 0.033 \\ -0.033 \end{pmatrix}$	

$$l_{,3} := \sum_{\text{liter} = 1}^{\text{NL}} \left(a_{\text{liter}} + \frac{d}{2} \right) \cdot 2 \cdot \pi \cdot \frac{la}{d}$$

$$l_{,3} = 1.357 \times 10^4$$

: mm total wire length

n := 1 .. NL + 1



del := 0.25001 **: [mm]**

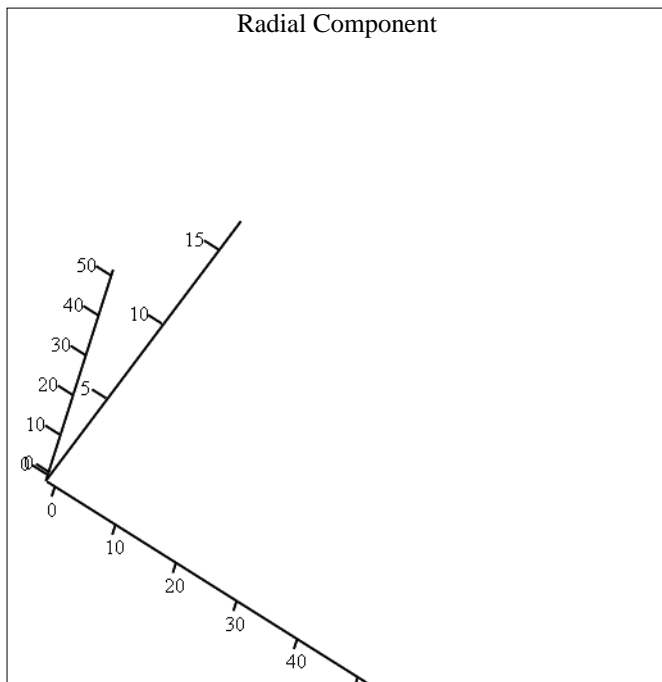
n := 0 .. 50

m := 0 .. 50

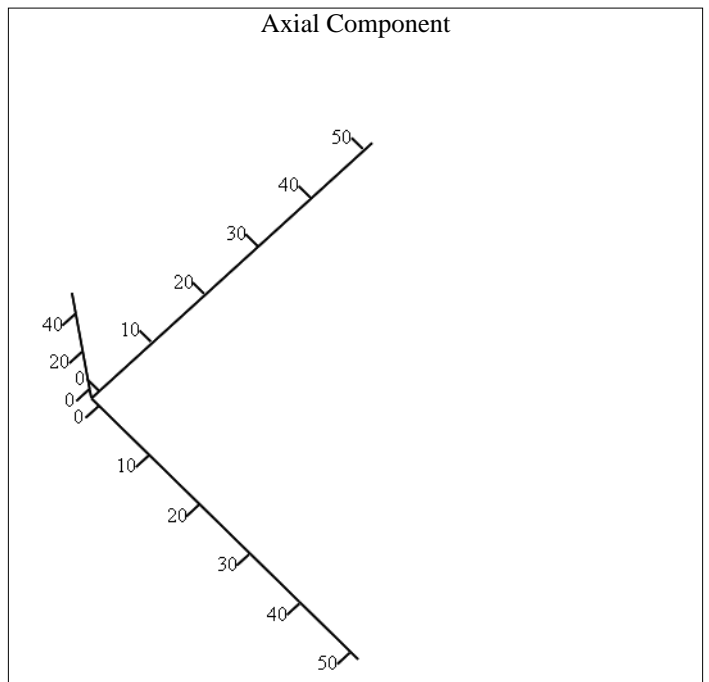
$$My_{n,m} := \sum_{\text{liter} = 1}^{\text{NL}} \text{BFy}(\text{del} \cdot n, \text{del} \cdot m, a_{\text{liter}}, la, l0)$$

$$Mz_{n,m} := \sum_{\text{liter} = 1}^{\text{NL}} \text{BFz}(\text{del} \cdot n, \text{del} \cdot m, a_{\text{liter}}, la, l0)$$

$$M_{n,m} := My_{n,m} + i \cdot Mz_{n,m}$$



My



Mz

M

Computation of the compressive force in k -Newton/meter= N/mm on the wire at the coil edge (radial unit: 0.25 mm):

liter := 1 .. 50 faradliter := Myliter, 40·10

farad_{liter}



liter

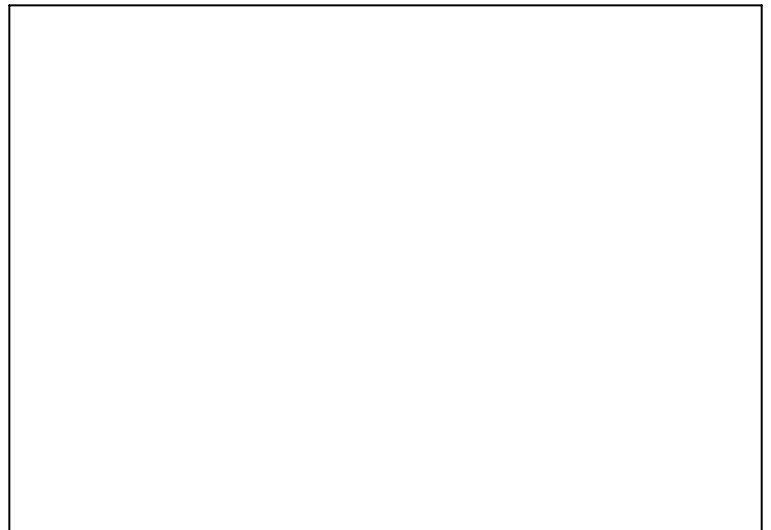
Computation of the axial force acting on the different layers:

m := 1 .. 20 r := 6, 8 .. 28

$$-f_m = \sum_{r=1}^{12} My_{4+2 \cdot r, m} \cdot 2 \cdot 10 \cdot a_r \cdot 2 \cdot \pi$$
: force produced by layer in position $z=0.25 \cdot m$ on the total of coil

: Newton

$-f_m$



m

Summation of all forces within one coil-half side:

$$\text{sum} := \sum_{n=1}^{20} -f_n$$
sum = ■
:Newton , total force of one coil-half

Computation of the inductance of the coil constructed by several layers of windings:

Length measurements in [mm], Induktivität in [Henry].

Height of the coil l_a [mm]

Radii of windings a_1, a_2 to be considered for cross inductance

Diameter of wire d [mm]

$l_a = \blacksquare$ $d = \blacksquare$

Number of windings per layer: l_a/d

$$L(a, b, L, d) := \frac{2 \cdot \pi \cdot 10^{-10} \cdot a \cdot b}{d^2} \cdot \int_0^{2 \cdot \pi} -\cos(\phi) \cdot \left[\int_{-\frac{L}{2}}^{\frac{L}{2}} \left[\ln \left[\frac{\left(\frac{L}{2} - z\right)^2 + \sqrt{\left(\frac{L}{2} - z\right)^2 + a^2 + b^2 + 2 \cdot a \cdot b \cdot \cos(\phi) + 10^{-5}}}{\sqrt{a^2 + b^2 + 2 \cdot a \cdot b \cdot \cos(\phi) + 10^{-5}}}} \right] \dots \right. \right. \\ \left. \left. + \ln \left[\frac{\left(\frac{L}{2} + z\right)^2 + \sqrt{\left(\frac{L}{2} + z\right)^2 + a^2 + b^2 + 2 \cdot a \cdot b \cdot \cos(\phi) + 10^{-5}}}{\sqrt{a^2 + b^2 + 2 \cdot a \cdot b \cdot \cos(\phi) + 10^{-5}}} \right] \right] dz$$

test result of present calculation:

$L(5, 5, 1000, 1) = \blacksquare$

Henry

classical result for "long" coil of one layer and 1000 windings

$4 \cdot \pi \cdot 10^{-7} \cdot 10^6 \cdot 25 \cdot \pi \cdot \frac{10^{-3}}{1000} = \blacksquare$

Henry

Computation of the inductance of the magnetic coil in consideration

$L_{teil}(i, j) := L(a_i \cdot 0.8, a_j \cdot 0.8, l_a, d)$

$NL = \blacksquare$

$L_{teil}(1, 1) = \blacksquare$

$L_{teil}(12, 12) = \blacksquare$

$Induk := \sum_{i=1}^{NL} \sum_{j=1}^{NL} L_{teil}(i, j)$

$Induk = \blacksquare$

:Henry

$m := 1 .. NL \quad n := 1 .. NL$

$ML_{m,n} := L_{teil}(m, n)$

ML = ■

Fixing of the system parameters:

coul := C2 coul = ■ **[Farad] capacity of the bank**

$\rho := 1.95 \cdot 10^{-6}$ **Ohm*cm at T=273 K** Lges := Induk

$\tau := \pi \cdot 1000 \cdot \sqrt{Lges \cdot coul}$ $\tau = \blacksquare$ **[msec] pulse length**

$\mu_0 := 4 \cdot \pi \cdot 10^{-9}$ **V*sec/A*cm**

Skin depth in wire:: $\delta_{RT} := \sqrt{0.2 \cdot \tau \cdot \frac{\rho}{\mu_0 \cdot \pi}}$ $\delta_{RT} = \blacksquare$ **[mm] Skin depth at T=273 K**

$R_{blind} := \sqrt{\frac{Lges}{coul}}$ $R_{blind} = \blacksquare$ **[Ohm] ratio of U/I**

$U_{max} := R_{blind} \cdot I_0$ $U_{max} = \blacksquare$ **[kV] Voltage for maximum field**

$\delta_{77} := \delta_{RT} \cdot \sqrt{0.13}$ $\delta_{77} = \blacksquare$ **[mm] skin depth at T=77 K**

$\delta_{He} := \delta_{RT} \cdot \sqrt{0.04}$ $\delta_{He} = \blacksquare$ **[mm] skin depth T=4.2 K**

**Calculation of temperature increase in coil after shot considering the "Action Integral" for a half-sinus current pulse of length τ and maximal current density j :
 $0.5 \cdot \tau \cdot j^2 = \text{Integral from starting temperature } T_{ex} \text{ before the shot to final temperature } T_f \text{ after pulse with length } \tau \text{ of integrand } [\rho d \cdot c(T) / \rho Cu]$
 ρd : density of Cu (not temperature dependent)
 $c(T)$ specific heat as function of temperature T**

$\rho_{Cu}(T)$ specific resistance as function of temperature T

Temperature dependence of the specific resistance of Cu: Data after HENNING (Fritz Herlach)

Resistance values:

$r_{16} := 1.0$ $r_{15} := 0.92$ $r_{14} := 0.68$ $r_{13} := 0.46$ $r_{12} := 0.23$ $r_{11} := 0.15$ $r_{10} := 0.065$
 $tesla_{16} := 273.0$ $tesla_{15} := 250.0$ $tesla_{14} := 200.0$ $tesla_{13} := 150.0$ $tesla_{12} := 100.0$ $tesla_{11} := 80.0$ $tesla_{10} := 60.0$
 $r_9 := 0.0195$ $r_8 := 0.014$ $r_7 := 0.0097$ $r_6 := 0.0074$ $r_5 := 0.0063$ $r_4 := 0.0057$ $r_3 := 0.005$
 $tesla_9 := 40.0$ $tesla_8 := 35.0$ $tesla_7 := 30.0$ $tesla_6 := 25.0$ $tesla_5 := 20.0$ $tesla_4 := 15.0$ $tesla_3 := 10.0$
 $r_2 := 0.0048$ $r_1 := 0.0044$ $r_0 := 0.004$
 $tesla_2 := 8.0$ $tesla_1 := 6.0$ $tesla_0 := 4.0$

$vs := cspline(tesla, r)$ $\rho_{cu}(T0) := interp(vs, tesla, r, T0) \cdot \rho$ **[Ohm*cm]**

Data after LANDOLT-BÖRNSTEIN:

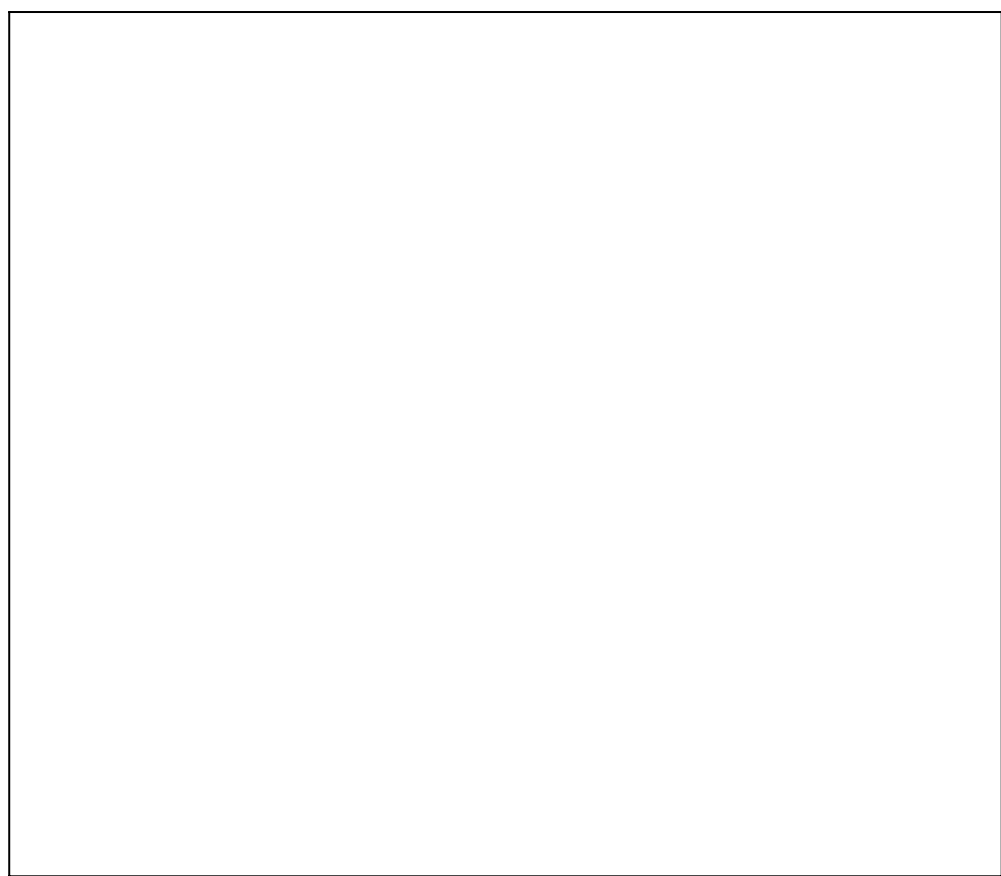
$q_0 := 0.0005$ $Tq_0 := 4$ $q_1 := 0.00016$ $Tq_1 := 14.558$ $q_2 := 0.00157$ $Tq_2 := 23.278$
 $q_3 := 0.00638$ $Tq_3 := 30.972$ $q_4 := 0.01380$ $Tq_4 := 36.80$ $q_5 := 0.02744$ $Tq_5 := 43.162$
 $q_6 := 0.04516$ $Tq_6 := 49.032$ $q_7 := 0.08050$ $Tq_7 := 57.528$ $q_8 := 0.12628$ $Tq_8 := 66.449$
 $q_9 := 0.16937$ $Tq_9 := 73.68$ $q_{10} := 0.24208$ $Tq_{10} := 84.921$ $q_{11} := 0.33307$ $Tq_{11} := 98.169$
 $q_{12} := 0.42132$ $Tq_{12} := 110.620$ $q_{13} := 0.46746$ $Tq_{13} := 117.178$ $q_{14} := 0.58023$ $Tq_{14} := 133.033$
 $q_{15} := 0.7191$ $Tq_{15} := 152.720$ $q_{16} := 0.8784$ $Tq_{16} := 175.55$ $q_{17} := 0.9687$ $Tq_{17} := 188.174$
 $q_{18} := 1.1017$ $Tq_{18} := 208.061$ $q_{19} := 1.3865$ $Tq_{19} := 250.187$ $q_{20} := 1.7055$ $Tq_{20} := 297.855$

$vsq := cspline(Tq, q)$ $\rho_{Cu}(T0) := interp(vsq, Tq, q, T0) \cdot 10^{-6}$ **[Ohm*cm]**

$T0 := 4, 5 .. 300$

■
 ρ_{cu}(T₀)
 ρ_{Cu}(T₀)
 0

: Ohm*cm



0 T₀ 300

Specific Heat after Debye:

$$c(T_0) := \left(\frac{T_0}{343}\right)^3 \cdot \left[\int_0^{\frac{343}{T_0}} \frac{x^4 \cdot e^x}{(e^x - 1)^2} dx \right] \cdot 1.2017$$

c(4.2) = ■

c(77) = ■

T₀ := 5, 6 .. 250

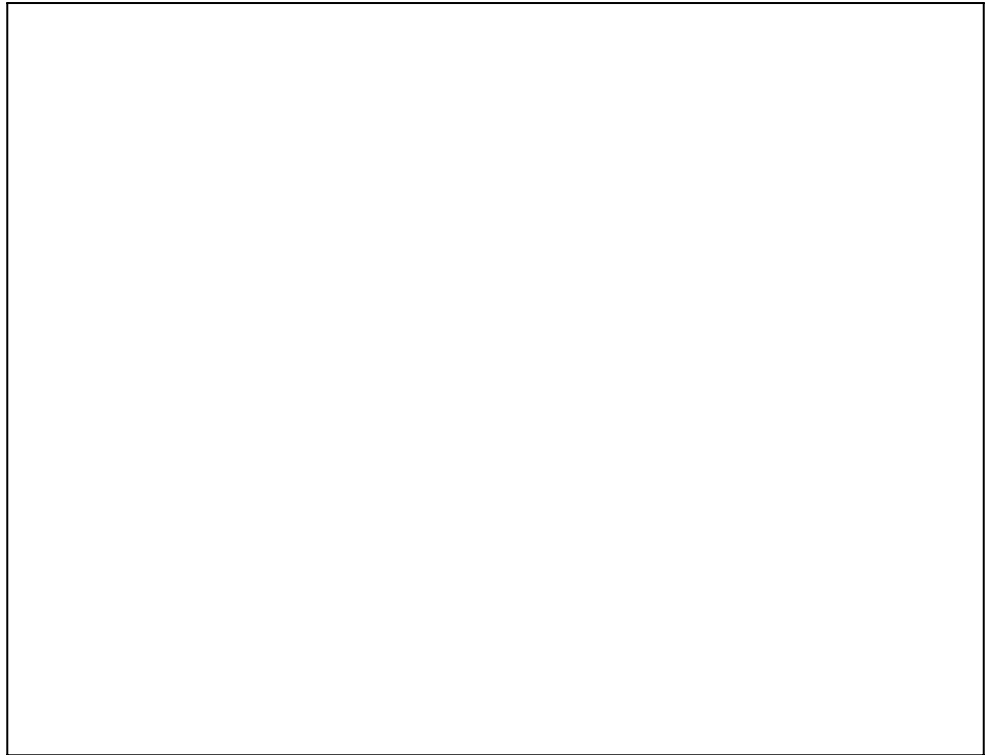
$$c(T0)$$

$$\rho_{cu}(T0) \cdot 10^5$$

$$\rho_{Cu}(T0) \cdot 10^5$$

$$c(T0) \cdot \frac{5}{\rho_{cu}(T0) \cdot 10^8}$$

$$c(T0) \cdot \frac{5}{\rho_{Cu}(T0) \cdot 10^8}$$



0 T0 250

Tex := 4.2 **[K] starting temperature of the coil before shot**

j = ■ **:maximum current density**

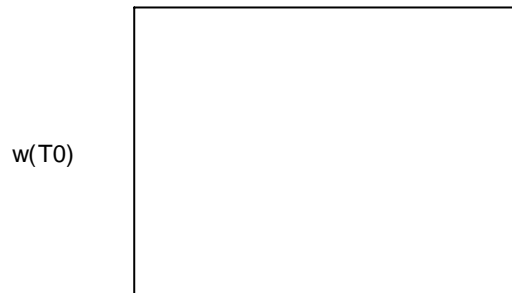
$$w(T0) := \int_{Tex}^{T0} \frac{c(\text{tesla})}{\rho_{Cu}(\text{tesla})} \text{ dtesla}$$

$$f := \frac{0.5 \cdot \tau \cdot j^2 \cdot 1.6501}{\rho d} \cdot 10^6$$

:Factor 1.6501 resulting from magneto resistance of the form: (1+0.00766*B(t)) [after Fritz HERLACH]

f = ■

T0 := 10, 40.. 500



0 T0 500

$$T_0 := 7$$

$$T_f := \text{root}\left(\frac{w(T_0)}{f} - 1, T_0\right)$$

$$T_f = \blacksquare$$

[K] final temperature of the coil after shot

$$T_{ex} := 77$$

[K] starting temperature of the coil before shot

$$j = \blacksquare$$

:maximum current density

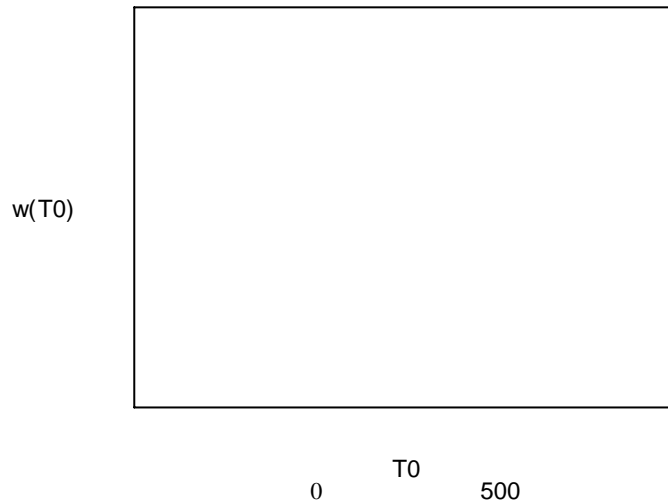
$$w(T_0) := \int_{T_{ex}}^{T_0} \frac{c(\text{tesla})}{\rho_{Cu}(\text{tesla})} d\text{tesla}$$

$$f := \frac{0.5 \cdot \tau \cdot j^2 \cdot 1.6501}{\rho d} \cdot 10^6$$

:Factor 1.6501 resulting from magneto resistance of the form: $(1+0.00766 \cdot B(t))$

$$f = \blacksquare$$

$$T_0 := 10, 40.. 500$$



$$T_0 := 100$$

$$T_f := \text{root}\left(\frac{w(T_0)}{f} - 1, T_0\right)$$

$$T_f = \blacksquare$$

[K] final temperature of the coil after shot

$d\phi$